

Coupling of MD with Continuum Mechanics via a Bridging Scale Approach

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Greg Wagner, Sandia National Laboratories







Collaborators

Northwestern University

Prof. Wing Kam Liu

Prof. Dong Qian (U. of Cincinnati)

Harold Park

Eduard Karpov

Hiroshi Kadowaki

Sulin Zhang

Prof. Shaofan Li (U.C.-Berkeley)

Sandia National Laboratories

Jonathan Zimmerman

Chris Kimmer

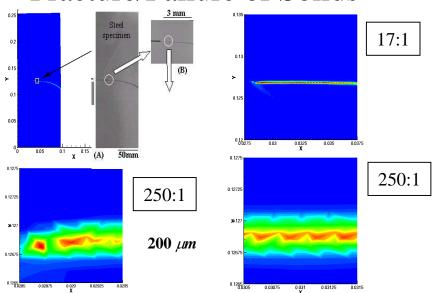
Reese Jones

Patrick Klein



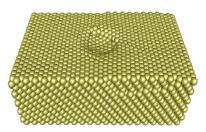
Examples of Multi-Scale Phenomena in Solids

Fracture/Failure of Solids



Prof. Shaofan Li, U.C.-Berkeley

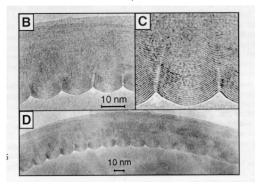
Nanoindentation



Dr. Eduard Karpov, Northwestern University

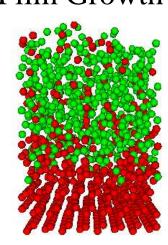
Nanoscale Devices

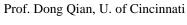
Poncharal et al., Science 283:1513





Film Growth









Concurrent Multiscales: Motivation

- Molecular dynamics simulations are limited to small domains (~10⁶-10⁸ atoms) and small time frames (~nanoseconds)
 - Experiments, even on nano-systems, involve much larger systems over longer times
- Continuum models are good, but not always adequate
 - Problems in fracture and failure of solids require improved constitutive models to describe material behavior
 - Molecular dynamics is required in regions of high deformation or discontinuity
- Multiple scale nature of these problems calls for a combined molecular dynamics/continuum mechanics approach





Concurrent Multiple Scales: Goals

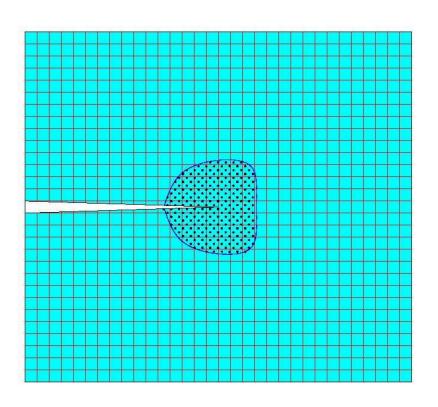
- Method for coupling molecular dynamics to finite element or meshfree computations in concurrent simulations
 - Simulation of time dependent, finite temperature problems
- True "coarse scale" discretization in continuum
 - No meshing down to atomic scale
 - Subcycling time-stepping algorithms to take advantage of multiple time scales
 - don't want to be limited to nano time scale everywhere in the domain
- Easy implementation
 - Re-use of existing MD and continuum codes
 - Easily parallelizable algorithms





Concurrent Coupled Simulations

- Molecular dynamics to be used in region of interest
 - near crack/shear band tip
 - inside shear band
 - at area of large deformation
 - around dislocations
 - etc.
- Finite elements/meshless "coarse scale" defined everywhere in domain
 - not just overlap/handshake region
- Bridging scale used to ensure FEM gives correct coarse scale behavior







- First, formally define exactly what is simulated at each scale
 - decompose total solution into coarse and fine scales
 - "bridging scale" used to represent the part of the total solution common to both simulations
 - provides coupling between the two simulations
- Second, eliminate fine scale degrees of freedom analytically outside of region of interest
 - use molecular dynamics (MD) only where necessary
 - use bridging scale decomposition to further define coupling between simulations
 - constitutive law in pure coarse scale region
 - boundary conditions on MD region



Coarse-Fine Decomposition

- Fields like displacement are decomposed into coarse and fine scales: $\mathbf{u} = \overline{\mathbf{u}} + \mathbf{u}'$
- Coarse scale is represented by smooth basis functions associated with nodes, e.g. finite element shape functions:

$$\overline{\mathbf{u}}(\mathbf{X}_{\alpha}) = \sum_{I} N_{I}(\mathbf{X}_{\alpha}) \mathbf{d}_{I} \xrightarrow{\text{matrix}} \overline{\mathbf{u}} = \mathbf{N}\mathbf{d}$$

– nodal degrees of freedom minimize mass-weighted error norm:

$$E = (\mathbf{u} - \mathbf{N}\mathbf{d})^{T} \mathbf{M}_{A} (\mathbf{u} - \mathbf{N}\mathbf{d})$$
$$\frac{dE}{d\mathbf{d}} = 0 \Rightarrow \mathbf{d} = (\mathbf{N}^{T} \mathbf{M}_{A} \mathbf{N})^{-1} \mathbf{N}^{T} \mathbf{M}_{A} \mathbf{u}$$

– This leads to a definition of the coarse scale in terms of a projection matrix: $\overline{\overline{u}=Pu}$

$$\mathbf{P} = \mathbf{N} (\mathbf{N}^T \mathbf{M}_A \mathbf{N})^{-1} \mathbf{N}^T \mathbf{M}_A$$



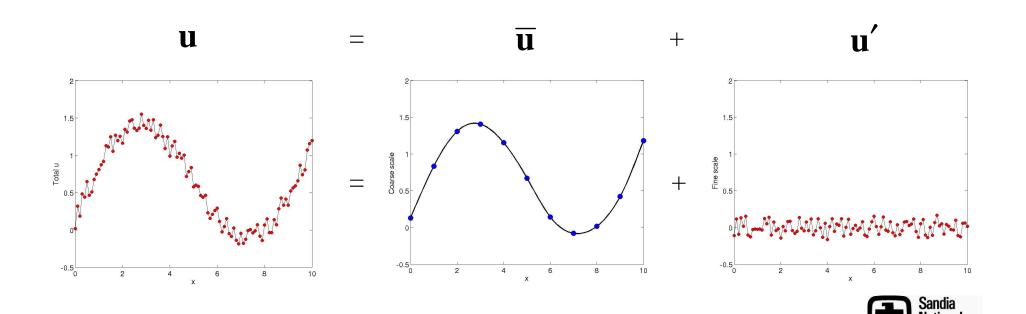
Coarse-Fine Decomposition

• Once coarse scale is defined, fine scale is "everything else":

$$u' = u - \overline{u}$$

$$= u - Pu$$

$$= (I - P)u \equiv Qu$$



Concurrent Multiscale Solution

 Use FEM for the coarse scale, MD for the fine scale in the decomposition:

$$\overline{u} = Nd \qquad \qquad \text{solve d using FEM} \\ u' = (I - P)q \qquad \qquad \text{solve q using MD}$$

• With our choice of projection operator, kinetic energy separates completely into coarse and fine scales:

$$K_E = \frac{1}{2}\dot{\mathbf{d}}^T \mathbf{M}\dot{\mathbf{d}} + \frac{1}{2}\dot{\mathbf{q}}^T \widetilde{\mathbf{M}}\dot{\mathbf{q}}$$

- Coupling between scales is only through the forcing term
 - Final momentum equations become:

Coarse scale:
$$\mathbf{M}\ddot{\mathbf{d}} = \mathbf{N}\mathbf{f}(\overline{\mathbf{u}} + \mathbf{u}')$$

Fine scale:
$$m_{\alpha}\ddot{\mathbf{q}}_{\alpha} = \mathbf{f}_{\alpha}(\overline{\mathbf{u}} + \mathbf{u}')$$

Reference: G. Wagner and W.K. Liu, *JCP* **190**:249-74 (2003).





Coarse Scale Modeling

 Coarse scale equation can be related to usual finite element treatment by approximating summations over atoms as domain integrals:

$$\sum_{J} \mathbf{M}_{IJ} \ddot{\mathbf{d}}_{J} = \mathbf{f}_{I} (\overline{\mathbf{u}}, \mathbf{u}')$$

where

$$\mathbf{M}_{IJ} = \int_{\Omega} \rho(\mathbf{x}) N_{I}(\mathbf{x}) N_{J}(\mathbf{x}) d\mathbf{x}$$

 The nodal force depends on the coarse scale only through the deformation gradient F:

$$\mathbf{f}_{I} = -\frac{\partial U}{\partial \mathbf{d}_{I}}$$

$$= -\sum_{\alpha} \frac{\partial W_{\alpha}}{\partial \mathbf{d}_{I}} \Delta V_{\alpha}$$

$$= -\sum_{\alpha} \frac{\partial \mathbf{F}_{\alpha}}{\partial \mathbf{d}_{I}} \frac{\partial W_{\alpha}}{\partial \mathbf{F}_{\alpha}^{T}} \Delta V_{\alpha} \approx -\int_{\Omega} N_{I,\mathbf{x}}(\mathbf{x}) \mathbf{P}^{K}(\mathbf{x}) dV$$





Fine Scale Boundary Conditions

- We want to avoid grading the coarse mesh down to the atomic lattice scale at the boundary
 - expensive
 - too much information
 - limits coarse scale time step
- Information passes from a fine MD lattice directly into a coarse scale mesh
 - small-scale energy can't be represented on the coarse scale, has nowhere else to go
 - leads to internal reflection of small scale waves
- Proper boundary treatment requires accounting for fine scale dynamics that are not simulated directly
 - correct boundary treatment falls out automatically from bridging scale decomposition
 - linearize in the fine scales at the boundary



MD Boundary Condition

$$\begin{vmatrix} \ddot{\mathbf{q}}_1(t) = \mathbf{M}_A^{-1} \mathbf{f}_1^*(t) + \int_0^t \mathbf{\theta}(t - \tau) \mathbf{a}_2'(\tau) d\tau + R_1(t) \\ \mathbf{a}_2'(t) = \mathbf{M}_{A2}^{-1} \mathbf{f}_2^*(t) - \ddot{\mathbf{u}}_2(t) \end{vmatrix}$$

Region 1: MD + FEM

Region 2: FEM only (+ "ghost atoms")

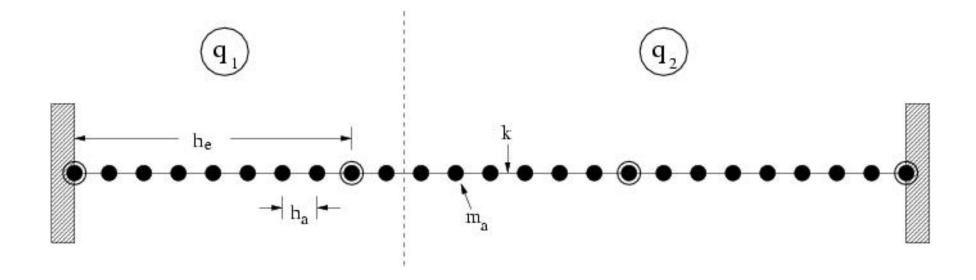
where $f^*(t)$ are forces computed using just the coarse scale displacements outside MD region (e.g. through "ghost atoms")

- The total forcing term consists of three major parts:
 - The standard interatomic force computed in MD simulation by assuming displacements of all atoms just outside the boundary are given by the coarse scale
 - A time history-dependent dissipation at the boundary (similar to a damping term)
 - A random forcing term at the boundary
 - the form of this term can be related to the temperature of the solid:

$$\langle R_i(t)R_j(0)\rangle = -\delta_{ij}\beta(t)k_BT$$



Example Problem: 1D Harmonic Chain

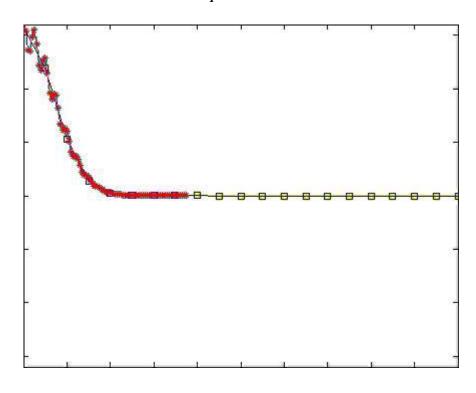


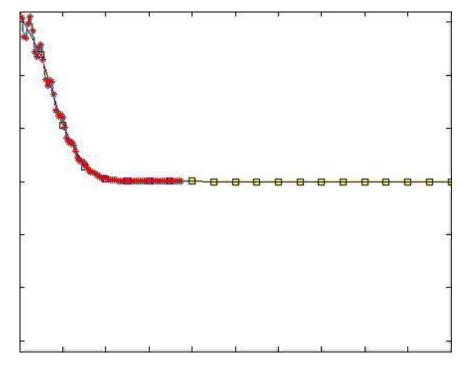


Effects of BC's on Internal Wave Reflection

$$\dot{\mathbf{q}}_{\alpha} = \sum_{I} N_{I} (\mathbf{x}_{\alpha}) \dot{\mathbf{d}}_{I}$$

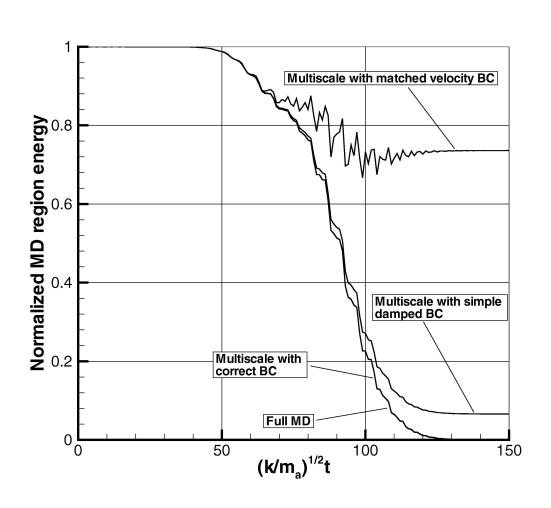
$$\ddot{\mathbf{q}}_1(t) = \mathbf{M}_A^{-1} \mathbf{f}_1^*(t) + \int_0^t \mathbf{\theta}(t - \tau) \mathbf{a}_2'(\tau) d\tau$$





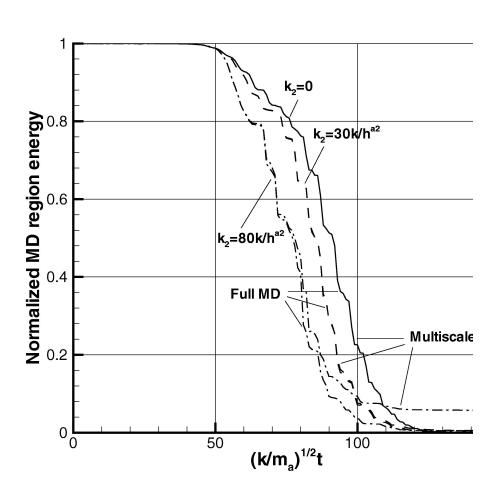


Energy Transfer out of MD Region





Energy Transfer out of MD Region: Nonlinear Potential



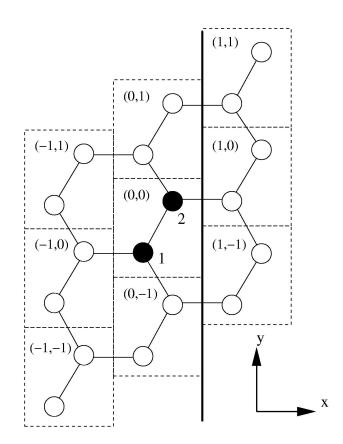


Damping Kernels in Multiple Dimensions

- Damping kernel can be easily computed for any regular crystal lattice across a planar boundary
 - periodicity allows spatial Fourier transform
 - unit cells can be indexed (*l*,*m*,*n*) in 3D, or (*l*,*m*) in 2D
 - boundary condition obtained by solving for atoms just outside boundary (*I*=1) in terms of atoms just inside boundary (*I*=0)
 - final boundary condition has form of time history integration with spatial coupling along boundary:

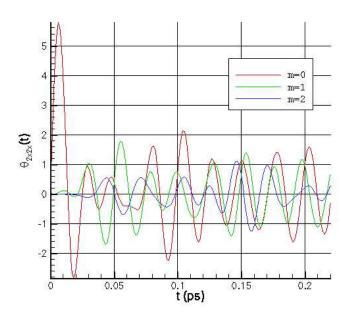
$$\mathbf{f}_{m}^{1\to 0}(t) = \sum_{m'=-\infty}^{\infty} \int_{0}^{t} \mathbf{\theta}_{m-m'}(t-\tau) \mathbf{u}_{0,m'}(\tau) d\tau$$

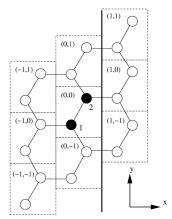
- note that \mathbf{u} and \mathbf{f} are vectors containing all dof's in the unit cell, and θ is a matrix coupling them
- Reference: G. Wagner, E. Karpov and W.K. Liu.
 Comp Meth. Appl. Mech. Eng., to appear (2004).

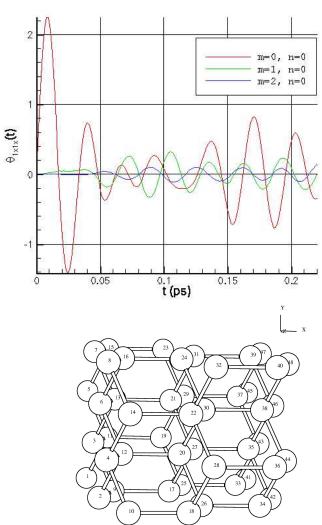




Damping Kernels in 3D: Carbon Structures







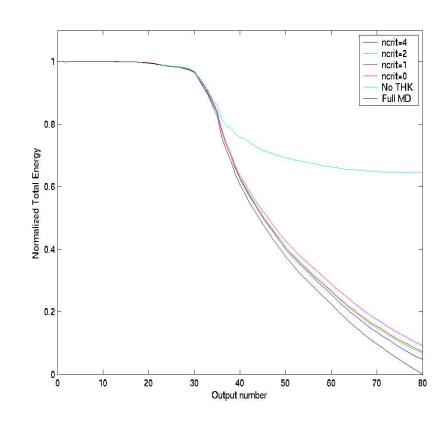




2D Multiscale Wave Propagation







Energy Transfer Rates:

No BC: 35.47%

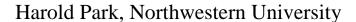
 $N_{crit} = 0$: 90.94%

 $N_{crit} = 1: 92.85\%$

 $N_{crit} = 2: 93.34\%$

 $N_{crit} = 4: 95.27\%$

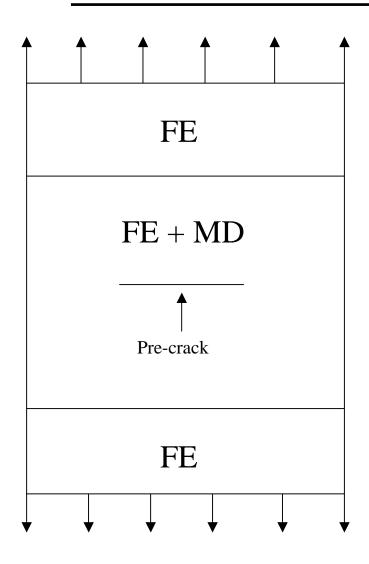
Full MD: 100%







2D Dynamic Crack Propagation



Problem Description:

- LJ 6-12 potential, σ = ϵ =1
- Nearest neighbor interactions
- 90000 atoms, 1800 finite elements (900 in coupled region)
 - •100 atoms per finite element
- $\Delta t_{fe} = 40 \Delta t_{md}$
- Ramp velocity BC on FEM
- Full MD = 180,000 atoms







Summary: Coupled MD/FEM

- Bridging scale decomposition allows concurrent simulation of fine scale using MD and coarse scale using FEM
 - bridging scale projection provides a unique decomposition of total solution for separation into coarse and fine scales
 - coarse scale mesh need not correspond to atomic lattice for coupling
 - subcycling can be used to take advantage of the different time scales in the coarse and fine regions
 - coarse scale equations and boundary conditions follow directly from the multi-scale formulation
- Future work:
 - study of approximations in boundary conditions
 - truncations of summations/integrals, approximations to kernel function
 - determination of most accurate/efficient integration of coarse scale region near MD boundary
 - development of coupled energy equation to track fine scale energy
 - time averaging as part of coarse scale projection

